## Health Risk Assessment Technical Support Document for Air Management Regulation VI Amendment

By

Air Management Services Department of Public Health City of Philadelphia June 16, 2021

#### I. List of Toxic Air Contaminants (Hazardous Air Pollutants)

The 1981 Air Management Regulation (AMR) VI lists 99 Toxic Air Contaminants (or Hazardous Air Pollutants (HAPs)). Over time, more air pollutants were found to cause cancer and other serious health effects. Under the 1990 federal Clean Air Act (CAA) Amendments, the original list of Hazardous Air Pollutants included 189 pollutants. Since then EPA has modified the list through rulemaking to include 187 HAPs <sup>[1]</sup>.

This AMR VI amendment aims to regulate an updated list of Toxic Air Contaminants originally in the Appendix to the 1981 AMR VI. The updated list of Toxic Air Contaminants (HAPs) is in the Appendix to the amended AMR VI. This list incorporates nearly all one hundred eighty seven (187) pollutants that are classified as hazardous air pollutants (HAPs) by U.S. EPA pursuant to Section 112 of the Clean Air Act, and includes additional air pollutants that have been determined to have adverse health effects by Air Management Service (AMS), taking into consideration the hazardous air pollutants listed by the New Jersey Department of Environmental Protection. It contains 217 chemical compounds and compound groups in total. The *Technical Guidelines for Air Management Regulation VI* document specifies the Reporting Threshold for each of chemical compounds (compound groups).

#### II. Establishing Hazardous Air Pollutants Reporting Thresholds

The objective of this section is to establish HAP Reporting Thresholds which can be used, as part of the AMS permitting process, in a health risk assessment to determine if there is the potential of HAP emissions to cause a significant health risk. A Reporting Threshold is an air pollutant emission rate (tons per year, or pounds per year) where The Philadelphia Department of Public Health (Department) has determined a health risk analysis is necessary. The methodology described below is used to determine the reporting thresholds. It is also used to establish the Risk Screening Workbook that will be used as a preliminary risk screening tool (also see Section III of *Technical Guidelines for Air Management Regulation VI*) in the permitting process. The methodology consists of the following three parts: Part 1: Modeling methodology; Part 2: Processing the modeling results; and Part 3: Identifying proposed threshold values.

#### 2.1 Modeling Methodology

Instead of setting a reporting threshold for each HAP in an arbitrary way, air quality modeling was used to estimate highly conservative or worst-case scenarios of allowable emission rates of a HAP at which the health risks caused by the pollutant concentrations can be kept at a level that is considered negligible. These highly conservative or worst-case scenario allowable emission rates provide the basis to establish the reporting threshold.

#### 2.1.1 Dispersion Model

A recent version of the American Meteorological Society/United States Environmental Protection

Agency Regulatory Model (AERMOD, Version 18081) was used for this evaluation. AERMOD is the US EPA preferred model for regulatory modeling applications. AERMOD is a steady-state plume model that incorporates air dispersion based on planetary boundary layer turbulence structure and scaling concepts, including treatment of both surface and elevated sources, and both simple and complex terrains.

#### 2.1.2 Land Use

To consider different land use types (dispersion environments) in Philadelphia, AERMOD was run in both the rural and urban modes. In the urban mode, a population parameter of 1,570,000 was used. This is approximately the population of the City of Philadelphia in 2017.

#### 2.1.3 Meteorological Data

Meteorological data sets include ground level weather observation data and upper air profile data. Data collected in the years 2010-2014 were used. The ground level data were the Philadelphia International Airport data sets; the concurrent upper air data were from the Sterling, Virginia station according to EPA air modeling protocols. Figure 1 shows the five-year wind rose based on ground level data from the Philadelphia International Airport weather station.



Figure 1: Wind Rose based on Philadelphia International Airport data

#### 2.1.4 Stack Parameters and Emission Rates

Hypothetical emission points and structures were entered into the model to represent a range of pollutant release and aerodynamic downwash scenarios for stacks. The stack parameters and emission rates used to generate the normalized air impact values (micrograms per cubic meter ( $\mu$ g/m<sup>3</sup>)/pound per hour of HAP emitted for short term impacts,  $\mu$ g/m<sup>3</sup>/ ton per year of HAP emitted for long term impacts) are listed in Table 1. The stack gas exit velocity and exit temperature values were selected so that plume rise would be minimal to provide highly conservative estimates. Emissions were assumed

to occur 24 hours per day, 365 days per year. Each modeled stack is located in the middle of a group of hypothetical buildings that are modeled for building downwash of the plume.

| Parameter                       | Value  |
|---------------------------------|--|
| Normalized Annual Emission Rate | 1 ton per year (normalized)                    |
| Normalized 1-Hour Emission Rate | 1 pound per hour (lb/hour) (normalized)        |
| Modeled Stack Heights (ft)      | 15, 20, 25, 30, 40, 50, 75, 100, 150, 200, 250 |
| Modeled Stack Diameter          | 1 foot   |
| Exit Velocity                   | 0.33 feet per second                           |
| Exit temperature                | 80 degrees Fahrenheit (°F)                     |

#### Table 1. Stack Parameters and Emission Rates

#### 2.1.5 Building Downwash

The building dimensions were selected so that the plume was subjected to aerodynamic downwash in all wind directions. The building dimensions used, including assumed horizontal dimensions, are listed in Table 2. To consider conservative plume downwash scenarios, all stacks were assumed below the Good Engineering Practice (GEP) stack height of 2.5 times the building height. For stack heights of 15 ft and 20 ft, the stack was assumed to be a factor of 1.25 times the building height. For all other stack heights (25 ft through 250 ft), the stack was assumed to be a factor of 1.5 times the building height. For stack heights between 15 and 50 ft, the building's horizontal dimensions were assumed constant at 50 ft. As stack heights increase above 50 ft, the building's horizontal dimensions also increase. The assumed building's horizontal dimensions are also shown in Table 2.

The US EPA's Building Profile Input Program (BPIP-PRIME) was used to generate building downwash parameters for input into AERMOD.

| Stack Height (ft) | Building Height (ft) | Building Width and Length (ft) |
|-------------------|----------------------|--------------------------------|
| 15                | 12                   | 50 x 50                        |
| 20                | 16                   | 50 x 50                        |
| 25                | 16.7                 | 50 x 50                        |
| 30                | 20                   | 50 x 50                        |
| 40                | 26.7                 | 50 x 50                        |
| 50                | 33.4                 | 50 x 50                        |
| 75                | 50                   | 75 x 75                        |
| 100               | 66.7                 | 100 x 100                      |
| 150               | 100                  | 150 x 150                      |
| 200               | 133.4                | 200 x 200                      |
| 250               | 166.7                | 200 x 200                      |

Table 2. Stack Heights and Assumed Building Dimensions

#### 2.1.6 Receptor Grid

Modeling was performed assuming flat terrain within the modeled distance range. A polar receptor grid with 864 receptors was used that was centered on the stack (midpoint of the buildings) with 36 radials spaced every 10 degrees. The spacing of receptors along the radials were as follows to provide 24 distances: 20 ft, 30 ft, 40 ft, 50 ft, 60 ft, 70 ft, 80 ft, 90 ft, 100 ft, 150 ft, 200 ft, 250 ft, 300 ft, 400 ft, 500 ft, 600 ft, 700 ft, 800 ft, 900 ft, 1000 ft, 1500 ft, 2500 ft, 3000 ft.

#### 2.1.7 Model Input and Output

The AERMOD model was run with EPA's regulatory default parameters and the parameters discussed above. AERMOD was run to calculate hourly, daily (24-hour), and annual concentrations at each receptor location.

#### 2.2 Processing Modeling Results

The above modeling methodology resulted in the following number of scenarios (impacts) being modeled:

2 dispersion environments x 5 sets of MET data x 2 normalized emission rates x 3 averaging times x 11 stack heights x 864 receptors = 570,240 impacts

In order to process such a large amount of data results, the AERMOD output files were reformatted and merged using a DOS batch processing script, then imported into Microsoft Excel. Statistical and pivot table functions in Excel were used to process the data. For each averaging time and each combination of stack height and receptor distance, the maximum normalized concentration was identified. For stack heights and distances not explicitly modeled (e.g. stack height 21 feet), linear interpolation across stack heights for a specified distance was performed to generate estimated concentration values. Similarly, concentrations at distances not explicitly modeled (e.g. 110 feet) were also estimated using linear interpolation.

Using this process, tables of worst-case hourly and annual impacts by stack height and distance were created for stacks from 15 ft to 250 ft and distances from 20 ft to 3,000 ft, including interpolated values. This resulted in 2,550 values in one table (Figure 2, normalized annual impacts). Each value represents the maximum concentration for a particular stack height and distance combination. However, for the purpose of setting HAP reporting threshold values, it is expected that the overall worst-case impacts will occur from shorter stacks at distances closer to the stack. Review of the AMS permitting and emission inventory data showed that at least 57% of approximately 1100 stacks (or release points) permitted in Philadelphia (not including small sources that are not reported in the emission inventories) are no more than 40 feet high. Of these stacks, at least 43% are located 150 feet

or less from the closest facility property line. Based on this analysis, only hourly and annual impacts for stacks <u>no more than 40 ft and within 150 ft</u> from the property line were considered. Again, this was meant to use more conservative scenarios in establishing reporting thresholds. In Figure 2, the area bounded by the blue box represents the subset of values used to establish the HAP reporting thresholds.

|      |              |         |         |            |            | 514         | ICK HAIGH | euro –  |         |        |         |         |         |          |        |           |          |             | Steck    |          | 0         |          |        |         |        |        |        |             |         |            |          | Steck Ha | Idea (Lat) |       |         |         |       |        |        |           |        |         |         |       | 50    | ACK HAIT | Twe (i.e) |       |       |
|------|--------------|---------|---------|------------|------------|-------------|-----------|---------|---------|--------|---------|---------|---------|----------|--------|-----------|----------|-------------|----------|----------|-----------|----------|--------|---------|--------|--------|--------|-------------|---------|------------|----------|----------|------------|-------|---------|---------|-------|--------|--------|-----------|--------|---------|---------|-------|-------|----------|-----------|-------|-------|
| Dirt |              |         |         |            |            |             |           |         |         |        |         |         |         |          |        |           |          |             |          |          |           |          |        |         |        |        |        |             |         |            |          |          |            |       |         |         |       |        |        |           |        |         |         |       |       |          |           |       |       |
|      |              |         |         |            |            |             |           |         |         |        |         |         |         |          |        |           |          |             |          |          | <b>1</b>  |          |        |         |        |        |        |             |         |            |          |          |            |       |         |         |       |        |        |           |        |         |         |       |       |          |           |       |       |
|      |              |         |         | 11         | 17 1       |             | 21        | 22      | 23      | 24     | 25      | 26      | 21      | 23       | 29     | 30        | 2 3      |             | 38       | 40       | 42        | 44       | 46     | 43      | 50     | 55     |        | <b>65</b> 7 |         | 5 20       |          |          | 75         | 100   | 110 1   | 20 1    | 30    | 140    | 50     | 160 170   |        | 20 1    | 178 4   | 200   | 210   | 220      | 230 2     |       | 250   |
|      | 0 43         | 850 4   | 1.61 3  | 3.652      | 37.553 35  | 454 33.35   | 5 33.326  | 34,436  | 35.067  | 35.631 | 36.208  | 34,866  | 33,524  | 32.182   | 30,840 | 23,433 2  | .621 2   | 5.156 23.84 | 5 22.01  | \$ 20.14 | 3 18.910  | J 10.600 | 16.443 | 15.210  | 13,911 | 12.333 | 10.689 | 3.045 r.    | 400 5   | 5.056 5.2  | Ur 4.65  | 8 4.109  | 3,560      | 3.011 | 2,651 2 | 232     | 1932  | 1572   | 1.212  | 1.037 0.3 | 981 L  | 3.865   | 0.750   | 0.634 | 0.583 | 0.531    | 0.480 (   | 3.428 | 0.311 |
|      | 20 43        | 650 4   | 1.61 3  | 3.652 0    | 31.553 35  | 454 33.35   | 5 33.326  | 34.436  | 35.067  | 35.631 | 36.208  | 34.866  | 33.524  | 32.182   | 30.840 | 23.433 2  | .621 2   | 5.156 23.8  | 5 22.01  | \$ 20.14 | 3 18.310  | J 10.60  | 16.443 | 15.210  | 13.911 | 12.333 | 10.689 | 3.045 r.    | 400 5   | 5.756 5.2  | Ur 4.65  | 8 4.109  | 3.560      | 3.011 | 2.651 2 | 232     | 1.932 | 1.572  | 1.212  | 1.097 0.3 | .981 L | 3.865   | 0.60    | 0.634 | 0.583 | 0.531    | 0.480 (   | 3.428 | 0.311 |
|      | 25 42        | 504 40  | 497 3   | 8.430 3    | 6.482 34   | .475 32.46  | 8 33.006  | 33.544  | 34.081  | 34.613 | 35.157  | 33.870  | 32.583  | 31.296   | 30.009 | 28.722 26 | .303 2   | 5.097 23.28 | 4 21.47  | 1 13.65  | 3 18.46   | 5 17.271 | 16.077 | 14.883  | 13.683 | 12.033 | 10.437 | 8,301 7     | .305 5  | 5.709 5.1  | 67 4.62  | 5 4.083  | 3.542      | 3.000 | 2.642 2 | .284    | 1.927 | 1.563  | 1.211  | 1.036 0.2 | .981 ( | J.865   | 0.750   | 0.634 | 0.583 | 0.531    | 0.480 (   | 0.423 | 0.377 |
|      | 30 4         | 158 39  | 243 3   | 37.327 3   | 35.412 33. | 496 31.58   | 1 32.086  | 32.591  | 33.096  | 33.601 | 34.107  | 32.874  | 31.642  | 30.410   | 29.178 | 27.346 2  | 5.191 24 | 437 22.68   | 3 20.92  | 8 19.17  | 4 18.020  | 0 16.865 | 15.711 | 14.557  | 13.402 | 11.854 | 10.306 | 8.757 7.    | 209 5   | 5.661 5.1  | 26 4.59  | 2 4.057  | 3.523      | 2.989 | 2.633 : | 2.277   | 1.922 | 1.566  | 1.210  | 1.035 0.9 | 380 C  | 0.865   | 0.750 ( | 0.634 | 0.583 | 0.532    | 0.480 0   | 0.429 | 0.378 |
|      | 35 39        | 485 31  | 1.677 3 | 5.869 3    | 34.061 32  | 254 30.44   | 5 30.914  | 31.382  | 31.850  | 32.318 | 32.785  | 31.618  | 30.451  | 29.284   | 28.117 | 26.350 25 | 268 23   | 3.587 21.9  | 5 20.22  | 4 18.54  | 2 17.436  | 5 16.330 | 15.224 | 14.118  | 13.012 | 11.526 | 10.041 | 8.556       | .071 5  | 5.586 5.0  | 63 4.53  | 9 4.015  | 3.492      | 2.968 | 2.616 2 | .264    | 1.912 | 1.560  | 1.208  | 1.093 0.5 | .978 0 | J.863 ( | 0.749 ( | 0.634 | 0.583 | 0.531    | 0.480     | 0.429 | 0.378 |
|      | 40 3         | .811 3  | 6.111 : | 34.411     | 32.711 3   | 1.011 29.31 | 1 29.742  | 30.173  | 30.603  | 31.034 | 31.464  | 30.362  | 29.260  | 28.158   | 27.056 | 25.354 24 | .346 23  | 2.737 21.12 | 8 19.51  | 9 17.9   | 11 16.853 | 3 15.795 | 14.737 | 13.679  | 12.621 | 11.199 | 9.777  | 8.355 6.    | 933     | 5.511 4.9  | 33 4.48  | 6 3.973  | 3.461      | 2.948 | 2.600   | 2.251   | 1.902 | 1.554  | 1.205  | 1.091 0.4 | .976 0 | J.862 ( | 0.748   | 0.633 | 0.582 | 0.531    | 0.480     | 0.429 | 0.378 |
|      | 45 36.       | 044 34  | .452 3  | 2.859 3    | 31.266 29  | .673 28.08  | 28.475    | 28.870  | 29.265  | 29.659 | 30.054  | 29.017  | 27.981  | 26.944   | 25.908 | 24.871 23 | .339 21  | 1.808 20.21 | 6 18.74  | 4 17.21  | 3 16.20   | 5 15.197 | 14,189 | 13.181  | 12.173 | 10.822 | 9.470  | 8.118 6     | .767 5  | 5.415 4.9  | 16 4.41  | 7 3.918  | 3.419      | 2.920 | 2.576 2 | 232     | 1.888 | 1.545  | 1.201  | 1.087 0.4 | .973 C | J.860 ( | 0.746   | 0.632 | 0.581 | 0.531    | 0.480     | 0.429 | 0.378 |
|      | 50 34        | 278 32  | .792 3  | 31.306 2   | 3.821 28   | .335 26.84  | 9 27.208  | 27.567  | 27.326  | 28.285 | 28.644  | 27.673  | 26.701  | 25.730   | 24.759 | 23.788 22 | .333 20  | 0.879 19.42 | 4 17.96  | 9 16.5   | 15.55     | 7 14.599 | 13.641 | 12.683  | 11.725 | 10.444 | 9,163  | 7.881 6.    | 600 5   | 5.319 4.8  | 33 4.34  | 8 3.863  | 3.377      | 2.892 | 2.553   | 2.214   | 1.875 | 1.535  | 1.196  | 1.083 0.7 | .970 ( | 0.857   | 0.744   | 0.631 | 0.581 | 0.530    | 0.479 0   | 0.428 | 0.377 |
|      | 55 32        | 596 31  | 206 2   | 29.815 2   | 8.425 27.  | 034 25.64   | \$ 25.972 | 26.301  | 26.623  | 26.957 | 27.286  | 26.374  | 25.461  | 24.549   | 23.637 | 22.724 2  | 343 19   | .962 18.5   | 31 17.20 | 0 15.81  | 9 14,908  | 3 13.997 | 13.086 | 12.175  | 11.264 | 10.052 | 8.841  | 7.629 6     | .418 5. | 5.206 4.7  | 37 4.26  | 7 3.797  | 3.327      | 2.857 | 2.524   | 2.191   | 1.857 | 1.524  | 1.190  | 1.078 0.5 | 966 r  | 0.854   | 0.742   | 0.630 | 0.579 | 0.529    | 0.478 0   | 0.428 | 0.377 |
|      | 60 30        | 915 29  | 620 2   | 8.324 2    | 7.029 25   | 734 24.43   | 8 24.736  | 25.034  | 25.332  | 25.630 | 25.328  | 25.075  | 24.221  | 23.368   | 22.514 | 21.661 20 | .353 19  | 046 17.73   | 8 16.43  | 0 15.12  | 2 14.258  | 8 13.394 | 12.530 | 11.666  | 10.802 | 3.661  | 8.519  | 7.377 6.    | 236 5   | 5.034 4.6  | 40 4.18  | 5 3.731  | 3.277      | 2.823 | 2.435   | 2.167   | 1.840 | 1.512  | 1.184  | 1.073 0.5 | 962    | 0.851 1 | 0.740   | 0.623 | 0.578 | 0.528    | 0.477     | 0.427 | 0.377 |
|      | 65 29.       | 124 28  | 203 2   | 6.993 2    | 25.778 24  | 563 23.34   | 8 23.620  | 23.893  | 24.165  | 24.437 | 24.709  | 23.905  | 23.101  | 22.297   | 21.492 | 20.688 1  | .445 18  | 203 16.96   | 0 15.71  | 7 14.41  | 5 13.652  | 2 12.829 | 12.007 | 11.184  | 10.361 | 9.283  | 8.205  | 7.127 6     | .050 4  | 4.972 4.5  | 34 4.03  | 6 3.658  | 3.220      | 2.782 | 2.461   | 2.140   | 1.819 | 1.498  | 1.177  | 1.067 0.  | .957 ( | 0.847   | 0.737   | 0.627 | 0.577 | 0.526    | 0.476 f   | 0.426 | 0.376 |
|      | 70 27.       | 332 26  | .797 2  | 5.662 2    | 4.527 23.  | 392 22.25   | 7 22.504  | 22.751  | 22.998  | 23.244 | 23.491  | 22.736  | 21.981  | 21.225   | 20.470 | 19,715 1  | .537 17  | .360 16.18  | 2 15.00  | 5 13.82  | 7 13.046  | 5 12.264 | 11.483 | 10,701  | 9.920  | 8,906  | 7.892  | 6.878 5     | 864 4   | .849 4.4;  | 28 4.00  | 6 3.585  | 3.163      | 2.742 | 2.427   | 2.113   | 1.799 | 1.484  | 1.170  | 1.061 0.1 | .952 r | 0.843   | 0.734   | 0.625 | 0.575 | 0.525    | 0.475     | 0.425 | 0.376 |
|      | 75 26.       | 586 25  | .613 2  | 24,541 2   | 3.468 22   | 395 21.32   | 2 21.547  | 21,772  | 21,338  | 22.223 | 22.448  | 21,732  | 21.015  | 20,299   | 19,583 | 18.866 1  | 744 1    | 5.621 15.43 | 9 14.37  | 5 13.25  | 3 12,508  | 8 11.763 | 11.019 | 10.274  | 3,523  | 8,567  | 7.606  | 6.645 5     | 684 4   | 4.723 4.3  | 18 3.91  | 3 3,507  | 3,102      | 2,697 | 2,390 2 | .083    | 1,776 | 1.468  | 1.161  | 1.053 0.7 | .946 r | 0.838   | 0.730   | 0.622 | 0.573 | 0.523    | 0.474 /   | 0.424 | 0.375 |
|      | 80 25        | 40 24   | 423 2   | 3.413 2    | 2.408 21   | 397 20.38   | 5 20 530  | 20,794  | 20,338  | 21,201 | 21405   | 20 728  | 20.050  | 19.373   | 18.635 | 18.018 1  | 350 15   | 882 14.8    | 5 13 74  | 7 12.67  | 9 11.97   | 1 11.263 | 10.554 | 3.846   | 3 137  | 8,229  | 7.321  | 6.412 5     | 504 4   | 1536 4.2   | 07 3.81  | 3 3.430  | 3.041      | 2.653 | 2,353 2 | 053     | 1753  | 1453   | 1.153  | 1046 07   | 939 (  | 0.833   | 0.726   | 0.620 | 0.571 | 0.522    | 0.472 /   | 0.423 | 0.374 |
|      | 85 24        | 398 23  | 434 2   | 2.463      | 21505 20   | 541 13.57   | 7 13.768  | 19.958  | 20.143  | 20.340 | 20.530  | 19.883  | 13,236  | 18,583   | 17.341 | 17.234 1  | 272 15   | 243 14.2    | 7 13.20  | 5 12.18  | 3 11.506  | 5 10.830 | 10.153 | 3.477   | 8.800  | 7.934  | 7.068  | 6,202 5     | 336 4   | 463 4.0    | 37 3.72  | 4 3.351  | 2.978      | 2.605 | 2.313 2 | 020     | 1728  | 1435   | 1.14.3 | 1038 0/   | 332 (  | 0.827   | 0.722   | 0.617 | 0.568 | 0.520    | 0.471     | 0.422 | 0.373 |
|      | 90 23        | 355 22  | 438 2   | 21520 2    | 0.603 19   | 685 18 76   | 8 18 945  | 19 123  | 19.300  | 19.478 | 19.655  | 19.038  | 18 4 21 | 17.804   | 17 187 | 16.570 1  | 593 1    | 616 13.64   | 0 12.66  | 3 1168   | 6 11.04   | 1 10.397 | 9.752  | 3 108   | 8463   | 7.639  | 6.815  | 5.991       | 167 4   | 343 3.9    | 86 3.62  | 9 3 272  | 2.915      | 2 558 | 2 273   | 988     | 1703  | 1.4.18 | 1133   | 1023 0    | 925 (  | 0.822   | 0.718   | 0.614 | 0.566 | 0.517    | 0.469     | 0.421 | 0.372 |
|      | 95 22        | 467 21  | 584 2   | 0 702      | 19.819 18  | 337 18.05   | 5 18 224  | 18 394  | 18 563  | 18 733 | 18 902  | 18 310  | 17 718  | 17 125   | 16 533 | 15.940 1  | 002 14   | 064 13.1    | 5 12 18  | 7 11 24  | 8 10.63   | 1 10.013 | 9.396  | 8 778   | 8 160  | 7 373  | 6 585  | 5,797 5     | 003 4   | 4 221 3 8  | 78 3.53  | 6 3 194  | 2.851      | 2 503 | 2 231   | 1954    | 1677  | 1400   | 1122   | 1020 0    | 918    | 0.815   | 0.713   | 0.611 | 0.563 | 0.515    | 0.467     | 0.419 | 0.371 |
|      | 00 01        | 578 20  | 730 1   | 9 883 1    | 9.036 18   | 189 17.34   | 1 17 503  | 17 665  | 17 8 96 | 17 988 | 18 14 9 | 17 580  | 17.014  | 16.4.4.6 | 15 878 | 15 310 1  | 1.411    | 3 511 10 6  | 11 11 71 | 1 10.8   | 10.000    | 9.630    | 9.039  | 8 4 4 8 | 7.858  | 7 106  | 6.354  | 5 6 0 2 4   | 850 4   | 099 33     | 71 3.44  | 3 3 115  | 9.787      | 2.460 | 2 190   | 920     | 1651  | 1381   | 1 111  | 1.011 0   | 910 (  | 0.809   | 0.709   | 0.608 | 0.560 | 0.513    | 0.465     | 0.418 | 0.370 |
|      | 10 20        | 363 19  | 567     | 18 771     | 17 974 17  | 178 16 38   | 0 16 501  | 16,659  | 16,797  | 16.935 | 17.074  | 16.54.9 | 16.010  | 15.478   | 14 946 | 14 414 11 | 564 1    | 0.715 11.86 | 6 11.01  | 7 10.16  | 8 9.610   | 9.057    | 8 501  | 7.945   | 7.390  | 6.693  | 5.996  | 5 300 4     | 603 3   | 906 3.5    | 98 3.99  | 0 2.982  | 2.673      | 2.400 | 2.109   | 1854    | 1598  | 1342   | 1086   | 0.989 0.0 | 892    | 0.794   | 0.697   | 0.599 | 0.553 | 0.507    | 0.460     | 0.414 | 0.367 |
|      | 20 19        | 140 10  | 402 1   | 17 6 5 9 1 | 16 942 46  | 16.0 10.000 | 0.045 520 | 10.000  | 45 76 9 | 45.000 | 45.000  | 10.546  | 15.005  | 14 509   | 14.040 | 10 517 1  | 249 4    | 1900 414    | 1 10 201 | 2 9.52   | 4 9.001   | 0.001    | 7.96.2 | 7.442   | 6.900  | 6 0.00 | 5.000  | 4 997 4     | 256 3   | 2 744 2 4  | 05 0.20  | 7 0.040  | 0.010      | 0.071 | 2,009   | 4 7 9 7 | 1.500 | 1202   | 1061   | 0.967 0.0 | 979    | 0.779   | 0.695   | 0.500 | 0.546 | 0.500    | 0.455     | 0.409 | 0.264 |
|      | 20 10        | 140 10  | 029 4   | 10.000     | 10.010 10  | 100 10.42   | 4 14 556  | 14 6 47 | 14,729  | 14.920 | 14,900  | 14 461  | 14.001  | 12 5 4 1 | 12.020 | 10.511    | 970 4    | 1104 10.2   | 7 960    | 0.02     | · 0.000   | 2 910    | 7.405  | 6.940   | 6 455  | 5 96 9 | 5.000  | 4.001 4     | 102 0   | 2.501 2.0  | ED 0.10  | 2 0.714  | 2.555      | 0.176 | 1949    | 1.101   | 1.343 | 1064   | 1.001  | 0.361 0.0 | 955    | 0.764   | 0.005   | 0.531 | 0.540 | 0.500    | 0.455 0   | 0.405 | 0.304 |
|      | 40 40        | 740 40  | 075 4   | 0.540      | 10.002 1.  | 440 40.50   | 40.530    | 14.041  | 14.100  | 40.770 | 19.022  | 14.401  | 40.007  | 10.541   | 10.000 | 12.020 1  | 006 40   | 1.124 10.3  | 0 0.02   | 0.00     | 0.330     | 2 2002   | 6.007  | 0.340   | 5.007  | 5.000  | 1.004  | 4.000 4     | .100 0  | 0.021 0.2  | 2 2.00   | 0 0.504  | 0.004      | 2.110 | 1.040   | 120     | 1402  | 1204   | 1.030  | 0.040 0.  | 000    | 0.740   | 0.015   | 0.505 | 0.550 | 0.404    | 0.450 0   | 0.405 | 0.001 |
|      |              | 110 10  | 015 1   | 15.433     | 14.131 14  | 140 13.50   | 0 10.514  | 10.042  | 10.110  | 10.110 | 10.040  | 10.421  | 12.331  | 12.512   | 12.140 | 10.003 4  | 026 10   | .523 5.63   | 2 0.33   | 0.23     | 0 1.100   | 0 1.001  | 0.001  | 5.401   | 5.500  | 5.450  | 4.324  | 4.002 0     | .001 3. |            | 00 2.00  | 0 2.501  | 2.331      | 2.002 | 1.001   | 1.000   | 1433  | 1.225  | 0.005  | 0.323 0.8 | 336 0  | 0.704   | 0.002   | 0.515 | 0.531 | 0.400    | 0.444     | 0.401 | 0.350 |
|      | 50 15        | 50.5 14 | .312 1  | 4.520      | 15.125 15  | 130 12.54   | 1 12.531  | 12.030  | 12.001  | 12.125 | 12.110  | 12.001  | 11.555  | 11.004   | 11.215 | 10.021 1  | 100 3    | 0.04 0.04   | 0.24     | 1 1.55   | 4 1.113   | 0.104    | 0.343  | 5,335   | 5.520  | 5.045  | 4.300  | 4.030 3     | .013 3  | 3.131 2.3  | 01 2.61  | 1 2.441  | 2.211      | 1.301 | 1.101   | 1.500   |       | 1.100  | 0.305  | 0.301 0.  | 010 0  | 0.104 0 | 0.650   | 0.566 | 0.524 | 0.402    | 0.433 0   | 0.331 | 0.355 |
|      | 60 13        | 505 K   | 5.165   | 12.725 1   | 2.285 11   | .845 11.40  | 5 11.358  | 11.311  | 11.264  | 11.217 | 11.170  | 10.891  | 10.623  | 10.349   | 10.076 | 3.802 3   | 232 8    | 5.782 8.2   | 2 1.16   | 2 6.25   | 2 6.862   | 2 6.472  | 6.082  | 5.632   | 5.302  | 4.841  | 4.380  | 3.920 3     | 453 2   | 2.338 2.6  | 82 2.56  | 6 2.343  | 2.133      | 1.317 | 1.625   | 1533    | 1342  | 1.150  | 0.353  | 0.878 0.0 | 138    | 0.00    | 0.631   | 0.556 | 0.515 | 0.474    | 0.433     | 0.331 | 0.350 |
| -    | 10 11        | 108 1   | L413    | 11.130 1   | 10.841 10  | 352 10.26   | \$ 10.125 | 3,381   | 3,848   | 9,109  | 3.511   | 3.412   | 3.254   | 3.035    | 8,336  | 5 111.8   | 404 8    | 5.031 r.6   | r r.28   | 4 6.3    | 0 6.543   | 5 6,180  | 5.815  | 5,443   | 5.084  | 4.633  | 4.134  | 3.650 3     | 305 2   | 2.860 2.6  | or 2.45  | 4 2.252  | 2.043      | 1.846 | 1.663   | 1.481   | 1238  | 1.115  | 0.332  | 0.855 0.  | 811    | 0.701 0 | 0.623   | 0.546 | 0.506 | 0.466    | 0.426 (   | J.386 | 0.346 |
| 1    | 80 3         | 810 9   | .6r2    | 3.535      | a.aar a.   | 260 3.12    | 2 8.832   | 8.662   | 8.432   | 8.202  | 1.311   | 1.328   | 1.884   | 1.840    | r.rar  | r.153     | r.516    | r.218 r.04  | 2 6.80   | 5 6.56   | 3 6.220   | 5 5.888  | 5.541  | 5.207   | 4.866  | 4.437  | 4.008  | 3.513       | 3.151 2 | 2.722 2.5  | 32 2.34  | 3 2.154  | 1.365      | 1.05  | 1.601   | 428     | 1.254 | 1.080  | 0.306  | 0.832 0.  | .058 0 | 3.684   | 0.610   | 0.536 | 0.491 | 0.458    | 0.419     | 0.381 | 0.342 |
| 1    | 90 7         | 312 7   | 326     | 7.340      | 7.353 7    | .367 7.38   | 1 7.653   | 7.337   | 7.015   | 6.634  | 6.372   | 6.443   | 6.515   | 6.586    | 6.657  | 6.728 6   | 628 6    | 528 6.4     | 7 6.32   | 7 6.22   | 7 5.31    | 1 5.585  | 5.280  | 4,364   | 4.648  | 4.235  | 3.822  | 3.409 2     | 336 2   | 2.583 2.4  | 08 2.23  | 2 2.056  | 1.880      | 1.705 | 1.540   | 1.375   | 1.210 | 1.045  | 0.880  | 0.809 0.9 | 738 0  | 3.667   | 0.536   | 0.526 | 0.488 | 0.450    | 0.413     | 0.375 | 0.337 |
| 2    | 00 6         | .015 6  | 5.179   | 6.344      | 6.503 6    | .674 6.83   | 5 6.426   | 6.012   | 5.533   | 5.186  | 4.172   | 4.353   | 5.145   | 5.331    | 5.518  | 5.704     | .740     | 5.776 5.8   | 2 5.84   | 9 5.88   | 5 5.584   | 5.303    | 5.012  | 4.721   | 4.431  | 4.033  | 3.636  | 3.239 2     | 842 2   | 2.445 2.2  | 83 2.12  | 1 1.958  | 1.736      | 1.634 | 1.478   | .322    | 1.166 | 1.010  | 0.854  | 0.786 0.  | .718   | 0.651   | 0.583   | 0.515 | 0.479 | 0.443    | 0.406     | 0.370 | 0.333 |
| 2    | 25 :         | 185 5   | 207     | 5.230      | 5.252 5    | .274 5.29   | 5 5.051   | 4.805   | 4.561   | 4.316  | 4.071   | 4.126   | 4.181   | 4.236    | 4.291  | 4.346 4   | 234 4    | .243 4.1    | 91 4.133 | 9 4.08   | 3,834     | \$ 3,700 | 3.507  | 3.314   | 3.120  | 2.943  | 2.767  | 2.590 2     | .413 2  | 2.237 2.0  | 88 1.94  | 0 1.792  | 1.644      | 1.435 | 1.356   | 1.216   | 1.076 | 0.937  | 0.797  | 0.735 0.9 | 014    | 0.612   | 0.551   | 0.489 | 0.456 | 0.422    | 0.388     | 0.355 | 0.321 |
| 2    | 50 4         | 356 4   | 236     | 4.115      | 3.994 3    | .874 3.75   | 3 3.677   | 3.600   | 3.524   | 3.447  | 3.370   | 3.294   | 3.218   | 3.141    | 3.065  | 2.988 2   | .849 2   | 2.709 2.56  | 9 2.43   | 2.25     | 0 2.194   | \$ 2.098 | 2.002  | 1.906   | 1.810  | 1.853  | 1.897  | 1.941 1     | 984 2   | 2.028 1.8  | 94 1.76  | 0 1.625  | 1.491      | 1.357 | 1.234   | 1.110   | 0.987 | 0.864  | 0.740  | 0.685 0.6 | 329 /  | 0.574   | 0.519 ( | 0.463 | 0.432 | 0.401    | 0.371     | 0.340 | 0.309 |
| 2    | 275 3        | 885 3   | 3.781   | 3.677      | 3.573 3    | .470 3.36   | 5 3.296   | 3.227   | 3.157   | 3.088  | 3.018   | 2.952   | 2.886   | 2.820    | 2.754  | 2.687     | .565 2   | .442 2.32   | 0 2.19   | 7 2.07   | 4 1.986   | 5 1.898  | 1.809  | 1.721   | 1.633  | 1.685  | 1.737  | 1.789 1     | .841 1  | 1.893 1.7  | 65 1.63  | 7 1.510  | 1.382      | 1.254 | 1.143   | 1.031   | 1.920 | 0.808  | 0.696  | 0.645 0.5 | .593 ( | 0.542   | 0.491 ( | 0.439 | 0.411 | 0.382    | 0.354     | 0.325 | 0.297 |
| 3    | <b>00</b> 3  | 413 3   | .326    | 3.239      | 3.152 3    | .065 2.97   | 8 2.916   | 2.853   | 2.791   | 2.729  | 2.666   | 2.610   | 2.554   | 2.498    | 2.442  | 2.386     | .281     | 2.175 2.01  | 0 1.96   | 4 1.85   | 9 1.778   | 3 1.698  | 1.617  | 1.537   | 1.456  | 1.516  | 1.577  | 1.637 1     | .697 1  | 1.758 1.6: | 36 1.51  | 5 1.394  | 1.273      | 1.152 | 1.052 0 | 0.952   | 0.852 | 0.752  | 0.652  | 0.605 0.  | .557   | 0.510   | 0.463   | 0.415 | 0.389 | 0.363    | 0.337     | 0.311 | 0.285 |
| 3    | 50 2         | 865 2   | .796    | 2.727      | 2.657 2    | .588 2.51   | 9 2.466   | 2.412   | 2.359   | 2.306  | 2.253   | 2.207   | 2.161   | 2.116    | 2.070  | 2.024     | .937     | 1.850 1.76  | 3 1.67   | 5 1.58   | 9 1.522   | 2 1.456  | 1.389  | 1.323   | 1.256  | 1.244  | 1.231  | 1.218 1     | .205 1  | 1.193 1.1  | 161 1.13 | 0 1.098  | 1.067      | 1.035 | 0.944 ( | 0.853   | 0.762 | 0.671  | 0.580  | 0.540 0.4 | 499 0  | 0.459   | 0.418   | 0.378 | 0.355 | 0.332    | 0.309 0   | 0.286 | 0.263 |
| 4    | 00 a         | .317 2  | 266     | 2.214      | 2.163      | 2.111 2.06  | 2.015     | 1.971   | 1.927   | 1.883  | 1.839   | 1.804   | 1.768   | 1.733    | 1.697  | 1.662     | .593     | 1.525 1.45  | 6 1.38   | 7 1.31   | 9 1.266   | 5 1.214  | 1.161  | 1.109   | 1.057  | 0.971  | 0.885  | 0.799 0     | .714 0. | 0.628 0.6  | 86 0.74  | 4 0.802  | 0.860      | 0.918 | 0.836   | 0.754   | 0.672 | 0.590  | 0.508  | 0.475 0.  | .441 0 | 3.408 ( | 0.374   | 0.341 | 0.321 | 0.301    | 0.281     | 0.261 | 0.241 |
| 4    | 50 2         | 005 1   | .965    | 1.324      | 1.884 1.   | 844 1.80    | 3 1.764   | 1.724   | 1.685   | 1.646  | 1.606   | 1.577   | 1.548   | 1.518    | 1.489  | 1.459     | 400 1    | 1.340 1.2   | 1.22     | 1 1.16   | 2 1.116   | 5 1.071  | 1.025  | 0.979   | 0.934  | 0.859  | 0.784  | 0.709 0     | .635 0  | 0.560 0.5  | 74 0.58  | 3 0.604  | 0.619      | 0.633 | 0.600 0 | 1.566   | 0.532 | 0.498  | 0.464  | 0.434 0.4 | 403 F  | 0.373 0 | 0.342   | 0.312 | 0.234 | 0.276    | 0.258     | 0.240 | 0.222 |
| 5    | <b>00</b> 1. | 593 1   | .664    | 1.635      | 1.605 1    | .576 1.54   | 7 1.512   | 1.477   | 1.443   | 1.408  | 1.374   | 1.350   | 1.327   | 1.304    | 1.280  | 1.257     | .207     | 1.156 1.10  | 6 1.05   | 5 1.00   | 5 0.366   | 5 0.327  | 0.889  | 0.850   | 0.811  | 0.747  | 0.683  | 0.620 0     | .556 0. | 0.432 0.4  | 63 0.43  | 5 0.406  | 0.378      | 0.349 | 0.363   | 0.377 0 | 1.392 | 0.406  | 0.420  | 0.332 0.1 | .365 C | J.338   | 0.310   | 0.283 | 0.267 | 0.251    | 0.235     | 0.219 | 0.203 |
| 5    | 50 1.        | 180 1   | .453    | 1.438      | 1.417 1    | .397 1.37   | 5 1.344   | 1.312   | 1.273   | 1.247  | 1.215   | 1.196   | 1.178   | 1.159    | 1.140  | 1.121     | .078 1   | 0.95        | 0 0.94   | 5 0.90   | 2 0.863   | 9 0.835  | 0.801  | 0.767   | 0.734  | 0.676  | 0.619  | 0.561 0     | 503 0.  | .446 0.4   | 19 0.39  | 2 0.366  | 0.339      | 0.312 | 0.328 ( | .345    | 0.361 | 0.377  | 0.394  | 0.367 0.  | .341   | 0.315 ( | 0.288 ( | 0.262 | 0.247 | 0.232    | 0.217     | 0.201 | 0.186 |
| 6    | 00 1.        | 266 1   | 254     | 1.242      | 1.230      | L217 1.20   | 5 1.175   | 1.146   | 1.116   | 1.086  | 1.057   | 1.042   | 1.028   | 1.014    | 1.000  | 0.386 0   | 348      | 0.911 0.81  | 4 0.83   | 7 0.80   | 0 0.77    | 1 0.742  | 0.714  | 0.685   | 0.656  | 0.605  | 0.554  | 0.503 0     | .451 0. | .400 0.3   | 75 0.35  | 0 0.325  | 0.300      | 0.275 | 0.294   | 0.312   | 0.331 | 0.349  | 0.368  | 0.342 0   | .317 ( | 0.291 ( | 0.266   | 0.240 | 0.226 | 0.212    | 0.198     | 0.184 | 0.170 |
| 6    | 50           | .121    | 1.114   | 1.107      | 1.099 1.   | 092 1.08    | 5 1.057   | 1.029   | 1.001   | 0.973  | 0.945   | 0.934   | 0.923   | 0.912    | 0.901  | 0.890     | .858 0   | .826 0.75   | 4 0.76   | 2 0.73   | 0 0.704   | \$ 0.678 | 0.652  | 0.626   | 0.600  | 0.553  | 0.507  | 0.460 0     | .413 0  | 0.367 0.3  | 44 0.32  | 0.299    | 0.276      | 0.253 | 0.262   | 0.271   | 0.279 | 0.288  | 0.297  | 0.282 0.1 | 268 /  | 0.253 ( | 0.239   | 0.225 | 0.212 | 0.199    | 0.186     | 0.173 | 0.160 |
| 7    | 00 0         | 976 0   | .974    | 0.971      | 0.969 0.   | 366 0.36    | \$ 0,938  | 0.912   | 0.886   | 0.859  | 0.833   | 0.825   | 0.817   | 0.810    | 0.802  | 0,794     | .767 0   | 0.740 0.7   | 4 0.68   | 7 0.66   | 0 0.63    | 7 0.614  | 0,590  | 0.567   | 0.544  | 0.502  | 0.460  | 0.417 0     | .375 0  | 0.333 0.3  | 13 0.29  | 2 0.272  | 0.252      | 0.232 | 0.231 0 | 229     | .228  | 0.227  | 0.226  | 0.222 0   | .219   | 0.216   | 0.212   | 0.209 | 0.197 | 0.185    | 0.173     | 0.161 | 0.143 |
| 7    | 50 O         | 874 0   | .874    | 0.873      | 0.873 0    | .872 0.87;  | 2 0.848   | 0.824   | 0,799   | 0.775  | 0.751   | 0.745   | 0,739   | 0.733    | 0.727  | 0.721 0   | 698 (    | 0.676 0.65  | 4 0.63   | 2 0.61   | 0 0.588   | 8 0.567  | 0.546  | 0.524   | 0.503  | 0.464  | 0.426  | 0.387 0     | 348 0   | 0.310 0.2  | 91 0.27  | 2 0.253  | 0.234      | 0.215 | 0.207   | 0,199   | 0,191 | 0.183  | 0,175  | 0.180 0   | .185   | 0,191   | 0.196   | 0.201 | 0.189 | 0.177    | 0.165     | 0.154 | 0.142 |
| 8    | 00 0         | 772 0   | 1773    | 0.775      | 0.777 0    | 778 0.78    | 0.758     | 0.736   | 0.713   | 0.691  | 0.663   | 0.665   | 0.660   | 0.656    | 0.652  | 0.647 0   | 630 1    | 0.612 0.53  | 4 0.57   | 7 0.55   | 9 0.540   | 0.520    | 0.501  | 0.481   | 0.462  | 0.427  | 0.392  | 0.357 0     | .321 0  | .286 0.2   | 69 0.25  | 0.233    | 0.216      | 0.198 | 0.183   | 0.169   | 0.154 | 0.140  | 0.125  | 0.133 0   | .152   | 0.165   | 0.179   | 0.192 | 0.181 | 0.169    | 0.158     | 0.146 | 0.135 |
| 8    | 50 0         | 721 (   | 0.719   | 0.716      | 0.714 0    | .712 0.70:  | 9 0.689   | 0.668   | 0.648   | 0.627  | 0.606   | 0.603   | 0.600   | 0.597    | 0.594  | 0.591     | 0.577 0  | 0.562 0.54  | 8 0.53   | 3 0.51   | 8 0.50    | 1 0.483  | 0.466  | 0.448   | 0.431  | 0.398  | 0.366  | 0.333 0     | .301 0  | 0.268 0.2  | 52 0.23  | 5 0.218  | 0.202      | 0.185 | 0.171   | 0.158   | 0.144 | 0.130  | 0.116  | 0.126 0   | .137   | 0.147   | 0.157   | 0.168 | 0.160 | 0.153    | 0.145     | 0.137 | 0.130 |
|      | 00 0         | 670 0   | 664     | 0.658      | 0.652 0    | 645 0.63    | 9 0.620   | 0.601   | 0.582   | 0.563  | 0.544   | 0.542   | 0.540   | 0.539    | 0.537  | 0.536     | 524      | 0.512 0.5   | 0.48     | 9 0.43   | 7 0462    | 0 4 4 6  | 0.431  | 0.415   | 0.400  | 0.370  | 0.340  | 0.310 0     | 280 0   | 1250 0.2   | 35 0.21  | 9 0.203  | 0.188      | 0.172 | 0.159   | 146     | 0.133 | 0.120  | 0.107  | 0.114 0   | 122    | 0.129   | 0.136   | 0.143 | 0.140 | 0.136    | 0.132     | 0.129 | 0.125 |
|      | 50 0         | 528 0   | .619    | 0.610      | 0.601 0    | 592 0 58    | 2 0.568   | 0.553   | 0.538   | 0.524  | 0.509   | 0.505   | 0.502   | 0.498    | 0.434  | 0.491     | 481 0    | 0.472 0.46  | 2 0.45   | 3 0.44   | 3 0,430   | 0.416    | 0.402  | 0.388   | 0.374  | 0.346  | 0.319  | 0.231 0     | 263 N   | 0.235 0.2  | 21 0.20  | 6 0,191  | 0.177      | 0.162 | 0.150   | 0.137   | 0.125 | 0.113  | 0.100  | 0.102 0   | 103    | 0.105   | 0.106   | 0.108 | 0.107 | 0.106    | 0.106     | 0.105 | 0.105 |
| 10   | 00 0         | 586 0   | 574     | 0.562      | 0.550 0    | 538 0.52    | 5 0.515   | 0.505   | 0.495   | 0.485  | 0.474   | 0.463   | 0.463   | 0.457    | 0.451  | 0.446     | 439 1    | 1431 0.42   | 4 0.41   | 7 0.40   | 3 0.33    | 7 0.385  | 0.373  | 0.360   | 0.348  | 0.323  | 0.237  | 0.272 0     | 246 0   | 0.221 0.2  | 07 0.13  | 3 0.179  | 0.166      | 0.152 | 0.140   | 1 12 9  | 0.117 | 0.105  | 0.094  | 0.083 0   | 085    | 0.081   | 0.076   | 0.072 | 0.074 | 0.077    | 0.073     | 0.082 | 0.084 |
| 15   | 00 0         | 328 0   | 399     | 0.316      | 0.309 0    | 303 0.29    | 7 0.296   | 0.296   | 0.295   | 0.295  | 0.294   | 0.287   | 0.279   | 0.272    | 0.265  | 0.257 0   | 248 0    | 239 0.25    | 9 0.22   | 0.40     | 1 0.20    | 7 0.202  | 0.198  | 0.194   | 0.190  | 0.179  | 0.168  | 0.157 0     | 146 0   | 0.135 0.1  | 27 0.10  | 9 0.111  | 0.103      | 0.095 | 0.087 ( | 079     | 0.071 | 0.064  | 0.056  | 0.053 0   | 050    | 0.047   | 0.045   | 0.042 | 0.040 | 0.039    | 0.037     | 0.036 | 0.034 |
| 20   | 00 0         | 204 0   | 203     | 0.202      | 0.200 0    | 199 0.19    | B 0.197   | 0.196   | 0.195   | 0.194  | 0.193   | 0.190   | 0.188   | 0.185    | 0.182  | 0.180     | 0.171 1  | 0.260 0.22  | 5 0.22   | 7 0.13   | 9 0.20    | 0.130    | 0.125  | 0.121   | 0.116  | 0.111  | 0.106  | 0.101 0     | 097 0   | 0.032 0.0  | 87 0.08  | 2 0.077  | 0.072      | 0.067 | 0.061 ( | 056     | 0.050 | 0.045  | 0.040  | 0.037 0   | 035 (  | 0.033   | 0.030   | 0.028 | 0.027 | 0.026    | 0.025     | 0.024 | 0.023 |
| 20   | 00 0         | 140 0   | 140     | 0.129      | 0.129 0    | 129 0.13    | 0.101     | 0.100   | 0.103   | 0.104  | 0.100   | 0.100   | 0.100   | 0.100    | 0.102  | 0.130     | 1 1 1 1  | 0.100 0.1   | 7 0.11   | 2 0.10   | 0.104     | 0.100    | 0.095  | 0.091   | 0.097  | 0.099  | 0.079  | 0.074 0     | 070 0   | 0.065 0.0  | 62 0.00  | 9 0.056  | 0.052      | 0.050 | 0.046 0 | 049     | 028   | 0.024  | 0.020  | 0.000 0.  | 097    | 0.005   | 0.000   | 0.021 | 0.020 | 0.020    | 0.019     | 0.019 | 0.017 |
| 20   | 00 0         | 10.2 0  | 102     | 0.103      | 0.103 0    | 100 0.10    | 0.130     | 0.101   | 0.101   | 0.100  | 0.105   | 0.104   | 0.099   | 0.099    | 0.099  | 0.038     | 0.95 0   | 0.000 0.0   | 0.00     | a 0.00   | 6 0.004   | 0.000    | 0.035  | 0.031   | 0.001  | 0.062  | 0.069  | 0.057 0     | 052 0   | 0.000 0.00 | 46 0.05  | 4 0.050  | 0.053      | 0.038 | 0.046 0 | 022     | 030   | 0.034  | 0.000  | 0.020 0.0 | 021 0  | 0.020   | 0.019   | 0.021 | 0.020 | 0.020    | 0.015     | 0.016 | 0.011 |
| - 30 |              | 100 0   |         | 0.100      | 0.102 0    | uva 0.10/   | a 0.102   | 0.102   | 0.101   | 0.101  | 0.101   | 0.100   | 0.000   | 0.000    | 0.000  | 0.030     | .000 0   | .000 0.0    | 0.00     | 0.00     | 0.004     | 3,000    | 0.011  | 0.014   | 0.011  | 0.001  | 0.002  | 0.001 0     | .000 0. |            | +0 0.04  | 4 U.042  | 0.040      | 0.030 | 0.000 0 | 0000    |       | 0.061  | 0.024  | 0.020 0.9 | wen v  | 2.050   | 0.010   | 0.011 | 0.010 | 0.010    | 0.010     | 0.014 | 0.014 |

Figure 2. Modeling Results (Annual) Table: maximum concentration for each combination of stack height and distance -- HAP reporting thresholds to be based on concentrations caused by stacks no more than 40 feet high and within a distance of no more than 150 feet from stack to property line

#### 2.3 Identifying Proposed Reporting Threshold Values

#### 2.3.1 Concentration Percentile-based Threshold Values

Rather than arbitrarily basing the proposed HAP reporting thresholds on a single stack height/property-line combination, a robust statistical approach was utilized. This approach considered all modeled stack height/property-line distance combinations predicted for stacks no more than 40 ft high and property lines no more than 150 ft from the stack. A percentage frequency distribution of the modeled impacts was evaluated. The resulting percentiles represent conservative concentration scenarios that could reasonably be expected to occur for multiple stack property-line combinations. This subset of data contains normalized air concentration values for more than 570 combinations of stack heights and receptor distances. To generate candidate values of HAP reporting thresholds, the 85<sup>th</sup>, 90<sup>th</sup>, 95<sup>th</sup> and 98<sup>th</sup> percentiles of the modeled concentrations of this dataset were evaluated. Figure 3 shows the distribution of modeled normalized annual impacts. A percentile identifies the normalized air concentration value where the percentage of modeled impacts in the dataset are less than the indicated air concentration value. Based on this chart, the 98th percentile of normalized annual concentrations is at 37.7  $\mu$ g/m<sup>3</sup> per ton/year pollutant emission, which represents a highly conservative scenario. Figures 4 shows the data table of combinations of stack height and distances with the 85<sup>th</sup>, 90<sup>th</sup>, 95<sup>th</sup> and 98<sup>th</sup> percentiles. They are 29.3, 31.6, 34.3 and 37.7 µg/m<sup>3</sup> per ton/year respectively.



Figure 3. Percentage distribution of normalized annual concentrations

|               |       |       |       |       |       |       |       |       |       | Stack H | eight (f | t)    |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Distance (ft) | 15    | 16    | 17    | 18    | 19    | 20    | 21    | 22    | 23    | 24      | 25       | 26    | 27    | 28    | 29    | 30    | 31    | 32    | 33    | 34    | 35    | 36    | 37    | 38    | 39    | 40    |
| 20            | 43.85 | 41.75 | 39.65 | 37.55 | 35.45 | 33.36 | 33.93 | 34.50 | 35.07 | 35.64   | 36.21    | 34.87 | 33.52 | 32.18 | 30.84 | 29.50 | 28.56 | 27.63 | 26.69 | 25.76 | 24.82 | 23.89 | 22.95 | 22.01 | 21.08 | 20.14 |
| 25            | 42.50 | 40.50 | 38.49 | 36.48 | 34.48 | 32.47 | 33.01 | 33.54 | 34.08 | 34.62   | 35.16    | 33.87 | 32.58 | 31.30 | 30.01 | 28.72 | 27.82 | 26.91 | 26.00 | 25.10 | 24.19 | 23.28 | 22.38 | 21.47 | 20.56 | 19.66 |
| 30            | 41.16 | 39.24 | 37.33 | 35.41 | 33.50 | 31.58 | 32.09 | 32.59 | 33.10 | 33.60   | 34.11    | 32.87 | 31.64 | 30.41 | 29.18 | 27.95 | 27.07 | 26.19 | 25.31 | 24.44 | 23.56 | 22.68 | 21.81 | 20.93 | 20.05 | 19.17 |
| 35            | 39.48 | 37.68 | 35.87 | 34.06 | 32.25 | 30.45 | 30.91 | 31.38 | 31.85 | 32.32   | 32.79    | 31.62 | 30.45 | 29.28 | 28.12 | 26.95 | 26.11 | 25.27 | 24.43 | 23.59 | 22.75 | 21.91 | 21.06 | 20.22 | 19.38 | 18.54 |
| 40            | 37.81 | 36.11 | 34.41 | 32.71 | 31.01 | 29.31 | 29.74 | 30.17 | 30.60 | 31.03   | 31.46    | 30.36 | 29.26 | 28.16 | 27.06 | 25.95 | 25.15 | 24.35 | 23.54 | 22.74 | 21.93 | 21.13 | 20.32 | 19.52 | 18.71 | 17.91 |
| 45            | 36.04 | 34.45 | 32.86 | 31.27 | 29.67 | 28.08 | 28.48 | 28.87 | 29.26 | 29.66   | 30.05    | 29.02 | 27.98 | 26.94 | 25.91 | 24.87 | 24.11 | 23.34 | 22.57 | 21.81 | 21.04 | 20.28 | 19.51 | 18.74 | 17.98 | 17.21 |
| 50            | 34.28 | 32.79 | 31.31 | 29.82 | 28.33 | 26.85 | 27.21 | 27.57 | 27.93 | 28.28   | 28.64    | 27.67 | 26.70 | 25.73 | 24.76 | 23.79 | 23.06 | 22.33 | 21.61 | 20.88 | 20.15 | 19.42 | 18.70 | 17.97 | 17.24 | 16.51 |
| 55            | 32.60 | 31.21 | 29.82 | 28.42 | 27.03 | 25.64 | 25.97 | 26.30 | 26.63 | 26.96   | 27.29    | 26.37 | 25.46 | 24.55 | 23.64 | 22.72 | 22.03 | 21.34 | 20.65 | 19.96 | 19.27 | 18.58 | 17.89 | 17.20 | 16.51 | 15.82 |
| 60            | 30.92 | 29.62 | 28.32 | 27.03 | 25.73 | 24.44 | 24.74 | 25.03 | 25.33 | 25.63   | 25.93    | 25.07 | 24.22 | 23.37 | 22.51 | 21.66 | 21.01 | 20.35 | 19.70 | 19.05 | 18.39 | 17.74 | 17.08 | 16.43 | 15.78 | 15.12 |
| 65            | 29.42 | 28.21 | 26.99 | 25.78 | 24.56 | 23.35 | 23.62 | 23.89 | 24.16 | 24.44   | 24.71    | 23.91 | 23.10 | 22.30 | 21.49 | 20.69 | 20.07 | 19.45 | 18.82 | 18.20 | 17.58 | 16.96 | 16.34 | 15.72 | 15.10 | 14.47 |
| 70            | 27.93 | 26.80 | 25.66 | 24.53 | 23.39 | 22.26 | 22.50 | 22.75 | 23.00 | 23.24   | 23.49    | 22.74 | 21.98 | 21.23 | 20.47 | 19.72 | 19.13 | 18.54 | 17.95 | 17.36 | 16.77 | 16.18 | 15.59 | 15.00 | 14.42 | 13.83 |
| 75            | 26.69 | 25.61 | 24.54 | 23.47 | 22.39 | 21.32 | 21.55 | 21.77 | 22.00 | 22.22   | 22.45    | 21.73 | 21.02 | 20.30 | 19.58 | 18.87 | 18.31 | 17.74 | 17.18 | 16.62 | 16.06 | 15.50 | 14.94 | 14.38 | 13.81 | 13.25 |
| 80            | 25.44 | 24.43 | 23.42 | 22.41 | 21.40 | 20.39 | 20.59 | 20.79 | 21.00 | 21.20   | 21.41    | 20.73 | 20.05 | 19.37 | 18.70 | 18.02 | 17.48 | 16.95 | 16.42 | 15.88 | 15.35 | 14.81 | 14.28 | 13.75 | 13.21 | 12.68 |
| 85            | 24.40 | 23.43 | 22.47 | 21.51 | 20.54 | 19.58 | 19.77 | 19.96 | 20.15 | 20.34   | 20.53    | 19.88 | 19.24 | 18.59 | 17.94 | 17.29 | 16.78 | 16.27 | 15.76 | 15.25 | 14.74 | 14.23 | 13.72 | 13.20 | 12.69 | 12.18 |
| 90            | 23.36 | 22.44 | 21.52 | 20.60 | 19.69 | 18.77 | 18.95 | 19.12 | 19.30 | 19.48   | 19.66    | 19.04 | 18.42 | 17.80 | 17.19 | 16.57 | 16.08 | 15.59 | 15.10 | 14.62 | 14.13 | 13.64 | 13.15 | 12.66 | 12.17 | 11.69 |
| 95            | 22.47 | 21.58 | 20.70 | 19.82 | 18.94 | 18.05 | 18.22 | 18.39 | 18.56 | 18.73   | 18.90    | 18.31 | 17.72 | 17.13 | 16.53 | 15.94 | 15.47 | 15.00 | 14.53 | 14.06 | 13.59 | 13.13 | 12.66 | 12.19 | 11.72 | 11.25 |
| 100           | 21.58 | 20.73 | 19.88 | 19.04 | 18.19 | 17.34 | 17.50 | 17.66 | 17.83 | 17.99   | 18.15    | 17.58 | 17.01 | 16.45 | 15.88 | 15.31 | 14.86 | 14.41 | 13.96 | 13.51 | 13.06 | 12.61 | 12.16 | 11.71 | 11.26 | 10.81 |
| 110           | 20.36 | 19.57 | 18.77 | 17.97 | 17.18 | 16.38 | 16.52 | 16.66 | 16.80 | 16.94   | 17.07    | 16.54 | 16.01 | 15.48 | 14.95 | 14.41 | 13.99 | 13.56 | 13.14 | 12.72 | 12.29 | 11.87 | 11.44 | 11.02 | 10.59 | 10.17 |
| 120           | 19.15 | 18.40 | 17.66 | 16.91 | 16.17 | 15.42 | 15.54 | 15.65 | 15.77 | 15.88   | 16.00    | 15.50 | 15.01 | 14.51 | 14.01 | 13.52 | 13.12 | 12.72 | 12.32 | 11.92 | 11.52 | 11.12 | 10.72 | 10.32 | 9.92  | 9.52  |
| 130           | 17.93 | 17.24 | 16.55 | 15.85 | 15.16 | 14.46 | 14.56 | 14.65 | 14.74 | 14.83   | 14.92    | 14.46 | 14.00 | 13.54 | 13.08 | 12.62 | 12.25 | 11.87 | 11.50 | 11.12 | 10.75 | 10.38 | 10.00 | 9.63  | 9.25  | 8.88  |
| 140           | 16.72 | 16.08 | 15.43 | 14.79 | 14.15 | 13.51 | 13.57 | 13.64 | 13.71 | 13.78   | 13.85    | 13.42 | 13.00 | 12.57 | 12.15 | 11.72 | 11.37 | 11.03 | 10.68 | 10.33 | 9.98  | 9.63  | 9.28  | 8.93  | 8.59  | 8.24  |
| 150           | 15.50 | 14.91 | 14.32 | 13.73 | 13.14 | 12.55 | 12.59 | 12.64 | 12.68 | 12.73   | 12.77    | 12.38 | 11.99 | 11.60 | 11.22 | 10.83 | 10.50 | 10.18 | 9.86  | 9.53  | 9.21  | 8.89  | 8.56  | 8.24  | 7.92  | 7.59  |

| Percentile: |       |  |  |  |  |  |  |
|-------------|-------|--|--|--|--|--|--|
| 98%         | 37.68 |  |  |  |  |  |  |
| 95%         | 34.28 |  |  |  |  |  |  |
| 90%         | 31.62 |  |  |  |  |  |  |
| 85%         | 29.31 |  |  |  |  |  |  |

Figure 4. Annual concentrations for stack height/property line distance combinations at the 85<sup>th</sup>, 90<sup>th</sup>, 95<sup>th</sup>, and 98<sup>th</sup> percentiles

Normalized hourly concentrations were processed in a similar way to evaluate short-term impacts.

#### 2.3.2 Evaluation Methodology

Equations 1 and 2 below were used to calculate proposed reporting thresholds for emissions of HAP with available inhalation exposure toxicity data <sup>[2]</sup>. The normalized annual air impact values (C' in the equations) were obtained from Figure 3. Impact values at the 85<sup>th</sup>, 90<sup>th</sup>, 95<sup>th</sup> and 98<sup>th</sup> percentiles were used in calculations. These percentile impact values represent the concentrations from multiple combinations of stack heights and distances to property line that are expected to occur in conservative scenarios when one ton per year of a HAP is emitted. Unit risk factors (URF) and reference concentrations (RfC) used in the equations are based on toxicity data from the latest updates of US EPA Integrated Risk Information System <sup>[3]</sup>, CalEPA Toxicity Criteria Database <sup>[4]</sup>, and Agency for Toxic Substances and Disease Registry "Minimal Risk Levels for Hazardous Substances" <sup>[5]</sup>. Refer to the Department's Risk Screening Workbook for the URF and the RfC values. Using the normalized annual impacts (C') and the HAP specific URF and/or RfC, the candidate value of the reporting threshold (Q) was calculated.

Cancer based Threshold

Equation 1: 
$$Q = \frac{CR}{URF \times C^2}$$

Non-Cancer based Threshold

Equation 2: 
$$Q = \frac{HQ \times RfC}{C}$$

where:

Q = maximum annual emission rate, ton/yr - Threshold  $CR = cancer risk; capped at1 x 10^{-6}$  URF = pollutant-specific inhalation <u>Unit Risk Factor</u>, (µg/m<sup>3</sup>)<sup>-1</sup>HQ = non-cancer risk Hazard Quotient; capped at 1

RfC = pollutant-specific <u>Reference Concentration</u>,  $\mu$ g/m<sup>3</sup>

C' = normalized annual concentration,  $(\mu g/m^3)/(ton/yr)$ ; for

example, use the value at 95th percentile.

#### 2.3.3 Risk Guidelines for the Proposed HAP Reporting Thresholds

The cancer risk (CR) guideline for a HAP from a single source was determined as a risk of less than or equal to **one in a million (0.000001)**. The non-cancer risk guideline for a HAP was determined as a Hazard Quotient **(HQ) less than or equal to one (1)**. Risks at and below these levels are considered negligible. Cancer risk-based threshold candidate values were compared to long-term non-cancer risk threshold candidate values for those HAPs that have both carcinogenic and non-carcinogenic impacts in order to select a more stringent value. These values were also analyzed to ensure that no threshold would cause a short-term non-cancer risk with HQ above 1 if a HAP has short-term non-cancer toxicology data available.

The following principles were followed to develop the HAP reporting thresholds.

- 1. The maximum HAP reporting threshold is capped at 2000 pounds per year for any HAP even if the calculations by Equation 1 or 2 give a value above 2000.
- 2. 13 HAPs have reporting thresholds based on short-term toxicity data as these either showed a non- negligible risk for a short-term exposure when compared to long-term values or do not have long-term toxicity data available. See Appendix A for this list.
- 3. Certain HAPs, such as arsenic, cadmium, and chromium, are listed as "Chemical Compound Groups" (classes). These listings are defined as including any unique chemical substance that contains the named chemical (i.e., antimony, arsenic, etc.) as part of that chemical's molecular structure. When a compound or subgroup is individually listed under a group, the reporting threshold for the compound or subgroup takes precedence over the threshold listed for the chemical group. Also, no individual compound or subgroup within a chemical group should have a higher reporting threshold than its chemical group.

Table 3 shows examples of HAPs with percentile-based candidate threshold values and how a value for the reporting threshold is proposed.

| НАР                  | Perc  | entile Based Tł | nresholds (Ibs/ | year) | Candidate Value for<br>Reporting Threshold<br>(lbs/year) |
|----------------------|-------|-----------------|-----------------|-------|--|
|                      | 85th  | 90th            | 95th            | 98th  |  |
| Benzene              | 8.7   | 8.1             | 7.5             | 6.8   | 7.0  |
| Carbon Tetrachloride | 11.4  | 10.5            | 9.7             | 8.8   | 9.0  |
| Chloroform           | 3     | 2.75            | 2.5             | 2.3   | 2.3  |
| Formaldehyde         | 5.3   | 4.9             | 4.5             | 4.1   | 4.0  |
| Hydrogen Fluoride    | 955   | 885             | 816             | 743   | 740  |
| Methyl Bromide       | 341   | 316             | 292             | 265   | 265  |
| Vinyl Chloride       | 7.8   | 7.2             | 6.6             | 6.0   | 6.0  |
| Vinyl Acetate        | 13647 | 12650           | 11669           | 10616 | 2000   |

#### Table 3. Examples of Proposed Reporting Thresholds

#### 2.3.4 Comparison with Current AMR VI Guidelines

The current AMR VI (1981) does not have HAP reporting thresholds. In the guideline document for this version of the regulation, however, recommended ambient concentrations were established for the HAPs. For comparison, the maximum ambient concentration for a HAP was calculated based on the new methodology described above (Section 2.3.2). For example, if a HAP has cancer Unit Risk Factor (URF) equal to 0.0000002 /( $\mu$ g/m<sup>3</sup>) and if the negligible cancer risk (CR) level is set at 0.000001 (1 in a million), the maximum ambient concentration of this HAP is: C = CR/URF = 0.000001 / 0.0000002 = 5 ( $\mu$ g/m<sup>3</sup>).

Table 4 shows examples of how the recommended ambient concentrations in the current AMR VI guidelines are compared with the maximum concentrations based on the new methodology.

| НАР                     | Current AMR VI<br>Annual Ambier | - Recommended<br>at Concentration | Max. Annual Concentration (µg/m3) based on new methodology cancer risk |  |  |  |  |  |
|-------------------------|---------------------------------|-----------------------------------|--|--|--|--|--|--|
|                         | (ppb)                           | (µg/m3)                           | at 1/million & non-cancer HQ at 1                                      |  |  |  |  |  |
| Benzene                 | 24                              | 76.6                              | 0.13   |  |  |  |  |  |
| Methyl Bromide          | 120                             | 466                               | 5.0  |  |  |  |  |  |
| Formaldehyde            | 4.8                             | 5.9                               | 0.077  |  |  |  |  |  |
| Carbon tetrachloride    | 12                              | 75.6                              | 0.17   |  |  |  |  |  |
| Chloroform              | 24                              | 116.8                             | 0.043  |  |  |  |  |  |
| Vinyl chloride          | 2.4                             | 6.1                               | 0.11   |  |  |  |  |  |
| Chromium/compounds (VI) |                                 | 0.12                              | 0.00008  |  |  |  |  |  |

 Table 4. Recommended ambient concentrations in current AMR VI (1981) guidelines compared with maximum concentrations based on new methodology

These and other comparisons indicate that the maximum HAP concentrations based on the new methodology, with the cancer risk limited at 1 in a million and the non-cancer HQ limited at 1, are much lower than the recommended ambient concentrations in the current AMR VI guidelines.

#### 2.3.5 Comparison with New Jersey Reporting Thresholds

The methodology used here to establish the reporting thresholds is very similar to that used by the New Jersey Department of Environmental Protection to determine HAPs reporting thresholds in the New

Jersey air toxics regulation. Understandably the threshold values selected for Philadelphia are quite similar to those in the New Hersey regulation, as shown in Table 5.

| НАР                  | Threshold Value based on<br>Philadelphia Scenarios<br>(Ibs/year, at 98 <sup>th</sup> percentile) | New Jersey<br>Reporting Threshold<br>(Ibs/year) |
|----------------------|--|---|
| Benzene              | 6.8  | 6   |
| Methyl bromide       | 265  | 230   |
| Formaldehyde         | 4.1  | 3.5   |
| Hydrogen fluoride    | 743  | 600   |
| Carbon tetrachloride | 8.8  | 8   |
| Chloroform           | 2.3  | 2   |
| Vinyl Acetate        | 2000   | 2000  |
| Vinyl Chloride       | 6  | 5   |
| Acetaldehyde         | 24   | 21  |

# Table 5. Example of Philadelphia HAP Reporting Thresholds Compared with New Jersey Thresholds Fille Fille

#### III. Risk Screening Workbook

The above-described methodology was also used in developing the *Risk Screening Workbook*. It is a Microsoft Excel workbook that calculates the worst-case scenario cancer and non-cancer risks based on user input data, built-in worst-case HAP concentrations derived from air quality modeling, and URF and RfC values of the HAPs. Therefore, it is an easy-to-use tool that simplifies the screening process for the permit applicant. See Section III of the *Technical Guidelines for Air Management Regulation VI* and the spreadsheet file for more information.

#### **References:**

- 1. US EPA HAP list: https://www.epa.gov/haps/initial-list-hazardous-air-pollutants-modifications
- 2. New Jersey DEP Guidance on Risk Assessment for Air Contaminant Emissions" (http://www.state.nj.us/dep/aqpp/downloads/techman/1003.pdf)
- 3. US EPA Integrated Risk Information System (IRIS, <u>www.epa.gov/iris</u>)
- 4. CalEPA Toxicity Criteria Database (oehha.ca.gov/tcdb/index.asp)
- 5. Agency for Toxic Substances and Disease Registry "Minimal Risk Levels for Hazardous Substances" (MRLs, <u>https://www.atsdr.cdc.gov/minimalrisklevels/index.html</u>).

### Appendix A

## List of Reporting Thresholds Based on Short-Term Toxicity Data

| CAS #   | Chemical Compound  | Proposed Threshold<br>(lbs/year) |
|---------|--|----------------------------------|
| 75150   | Carbon disulfide   | 2000                             |
| 75003   | Ethyl chloride   | 2000                             |
| 111762  | Ethylene glycol monobutyl ether                          | 2000                             |
| 110805  | Ethylene glycol monoethyl ether (2-Ethoxy ethanol)       | 1800                             |
| 111159  | Ethylene glycol monoethyl ether acetate                  | 685                              |
| 109864  | Ethylene glycol monomethyl ether (2-<br>Methoxy ethanol) | 455                              |
| 7783075 | Hydrogen selenide  | 25                               |
|         | Manganese and compounds                                  | 0.8                              |
| 67561   | Methanol   | 2000                             |
| 71556   | Methyl chloroform  | 2000                             |
| 108101  | Methyl isobutyl ketone                                   | 2000                             |
| 108883  | Toluene  | 2000                             |
| 79016   | Trichloroethylene  | 10                               |